TRB Annual Meeting

A feedback control strategy for traffic flow harmonization in mixed-traffic environments --Manuscript Draft--

Full Title:	A feedback control strategy for traffic flow harmonization in mixed-traffic environments
Abstract:	Autonomous driving systems present promising methods for congestion mitigation in mixed autonomy traffic control settings. In particular, when coupled with even modest traffic state estimates, such systems can plan and coordinate the behaviors of automated vehicles (AVs) in response to observed downstream events, thereby inhibiting the continued propagation of congestion. In this paper, we present a simple feedback control strategy that exploits average speed estimates to mitigate the evolution of stop-and-go traffic in decentralized mixed-autonomy settings. Within this paradigm, our controller assigns desired speeds to automated vehicles that 1) predicatively react to the downstream state of traffic while 2) maintaining safe and reasonable headways with leading vehicles. This method is demonstrated to achieve an average of over 15% energy savings within simulations of congested events observed in Interstate I-24 with only 4% AV penetration, while restricting negative externalities imposed on traveling times and mobility.
Manuscript Classifications:	Operations; Vehicle-Highway Automation ACP30; Automated Vehicles; Connected Vehicles; Cooperative
Manuscript Number:	
Article Type:	Presentation
Order of Authors:	Zhe Fu
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Additional Information:	
Question	Response
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1 A FEEDBACK CONTROL STRATEGY FOR TRAFFIC FLOW HARMONIZATION IN **MIXED-TRAFFIC ENVIRONMENTS** Zhe Fu, Corresponding Author zhefu@berkeley.edu Abdul Rahman Kreidieh aboudy@berkeley.edu 12 Alexandre M. Bayen bayen@berkeley.edu Word Count: 5157 words + 3 table(s) \times 250 = 5907 words Submission Date: August 1, 2022

1 ABSTRACT

- 2 Autonomous driving systems present promising methods for congestion mitigation in mixed auton-
- 3 omy traffic control settings. In particular, when coupled with even modest traffic state estimates,
- 4 such systems can plan and coordinate the behaviors of automated vehicles (AVs) in response to
- 5 observed downstream events, thereby inhibiting the continued propagation of congestion. In this
- 6 paper, we present a simple feedback control strategy that exploits average speed estimates to mit-
- 7 igate the evolution of stop-and-go traffic in decentralized mixed-autonomy settings. Within this8 paradigm, our controller assigns desired speeds to automated vehicles that 1) predicatively react
- 9 to the downstream state of traffic while 2) maintaining safe and reasonable headways with leading
- vehicles. This method is demonstrated to achieve an average of over 15% energy savings within
- simulations of congested events observed in Interstate I-24 with only 4% AV penetration, while
- 12 restricting negative externalities imposed on traveling times and mobility.
- 13
- 14 Keywords: Mixed-autonomy traffic, Traffic control, Highway speed harmonization

2

1 INTRODUCTION

2 Vehicle autonomy is rapidly becoming a viable feature of many road networks. Early demon-3 strations in vehicle platooning (1-3) and similar successes spurred on by ambitious driving chal-4 lenges (4, 5) have motivated equally ambitious efforts in the industrial sector, with companies 5 including Tesla (6), Google (7), GM (8), and others all attempting to push the limitations and 6 scope of vehicle autonomy. This trajectory is expected to continue as well, with studies projecting 7 and discussing the implications of autonomy in the vicinity of 20-40% by 2050 (9).

The developments in vehicle autonomy, coupled with similar progressions in the prolifer-8 9 ation of connectivity (10), have enabled researchers and practitioners to ask interesting questions 10 on the quality of implemented driving policies. In particular, through carefully defined control and planning architectures, scientists have aimed to identify methods for reducing the energy foot-11 print of future automated vehicles (AVs). This research has taken multiple interesting forms, and 12 has ranged in scale from the macroscopic eco-routing of AVs (11, 12) to the sub-microscopic 13 planning of powertrain systems in response to gear-shifting behaviors (13, 14) and network topol-14 ogy (15, 16). 15

16 In this paper, we are interested primarily in the role of *longitudinal* driving behaviors on the energy-efficiency of a given network. This is a topic that has formerly been heavily explored in 17 the context of platoons of connected and automated vehicles, whereby platoons of fully-automated 18 vehicles have successfully maintained string-stable driving responses in tight platoons, thereby 19 providing notable benefits to both energy-efficiency and throughput. More relevant to the present 20 paper, however, AVs in mixed-autonomy setting may provide significant benefits in mitigating 21 string-instabilities among human drivers as well. This was demonstrated empirically in the seminal 22 23 work of (17), whereby a single AV within a circular track stably operating near the effectively uniform driving speed of the network manages to dampen stop-and-go oscillations existing prior 24 25 to actuation.

The above empirical study provides a useful insight that is frequently parroted (18, 19): 26 significant gains to energy-efficiency may be achieved by harmonizing the speeds of subsets of ve-27 hicles near a desirable target. This deduction, however, introduces new challenges to autonomous 28 driving systems. In particular, under the every-evolving dynamics of a particular network as de-29 30 mand waxes and wanes, AVs must reactively identify desirable speeds that match current spatiotemporal trends while not inhibiting the safety or mobility of the vehicle. To this, traffic state 31 estimates may offer a helping hand. Estimates of flow, density, and speed produced either from 32 fixed sensors or probe vehicles (20) may elucidate spatio-temporal patterns that may be exploited 33 by AVs in a largely decentralized manner. This is in part demonstrated in the work of (21), for in-34 35 stance, with devises an optimal speed profile for vehicles provided speed measurements forwards in space and time. Solutions such as these, however, are often studied in the context of fully-36 37 observable macroscopic environment, and as such become brittle and unsafe in the presence of inaccurate traffic state estimates and microscopic fluctuations in speed and spacing. 38

In this paper, we present a feedback control strategy that exploits both macroscopic traffictate estimates and microscopic observations to produce a reasonable car-following response while also attempts to harmonizing driving speeds across a desirable spatio-temporal target. The key contributions of this paper are as follows:

We construct a simple longitudinal feedback control strategy for AVs that attempts to maintain reasonable headways with preceding vehicles when appropriate, and adjusts its spacing when sudden reductions in driving speeds are anticipated in the near future.



FIGURE 1: An illustration of the targeted highway network within this study (I-24 Westbound in Nashville, Tennessee), seen as the red diagonal line within the highlight region.

We validate the efficacy of the above method on a simulation of throughput-restricted traffic aimed at capturing the high degree of variability in driving behaviors and traffic state estimates common to real-world networks, and demonstrate that our method can consistently achieve large energy savings in congested states of traffic.

5 PROBLEM STATEMENT

In this paper, we are interested in exploring methods for ameliorating congestion in mixed au-6 tonomy highway networks. The considered network, see Figure 1, is a 14.5-km long segment of 7 8 Interstate I-24 located in Nashville, Tennessee. This network has been the topic of some interest in recent years, with researchers attempting to both reconstruct (22, 23) and address (23-25) 9 characteristic of driving within this network that produce inefficiencies in energy consumption. 10 In particular, we here explore the implications of automated driving on addressing inefficiencies 11 arising from string instabilities in human driving behaviors, which result in the formation of stop-12 and-go traffic during peak demand intervals within this network. 13

To validate the efficacy of our longitudinal driving strategy within the I-24, we utilize a 14 microsimulation model presented in (23). In particular, to capture a degree of variability in driving 15 behaviors that is difficult to recreate with common microsimulation tools (26, 27), we instead 16 model the platoon response of both simulated human-driven and automated vehicles following 17 leading trajectories collected directly from the target network. These leading trajectories consist 18 of position and velocity measurements $\tau := \{(x_1, v_1), \ldots, (x_T, v_T)\}$ sampled in increments of 0.1 19 seconds, and vary in terms of time collected and severity of congestion witnessed, and as such 20 21 offer a robust assessment of the influence of automated vehicles within viable states of traffic.

To model the behaviors of platoons of vehicles following the aforementioned trajectories, we initially place *N* vehicles upstream of the leading vehicle and equidistant from one another¹, and update the state of said vehicles via logic specified either by a car-following model $f_{human}(\cdot)$

¹Vehicles are initially placed with 2-second gaps between one another and driving with the same speed as the leading vehicle.

Parameter	v_0	Т	а	b	δ	s_0	ε
Value	45	1	1.3	2.0	4	2	$\mathcal{N}(0, 0.3)$

TABLE 1: Intelligent Driver Model (IDM) Parameters

1 or the AV model described in the following section. For human-driven vehicles, this acceleration

2 response is dictated by the *Intelligent Driver Model* (28) (IDM), a popular model for reconstructing

3 string instabilities and the formation of stop-and-go style behaviors. Through this model, the

4 acceleration for a vehicle α is defined by its bumper-to-bumper space headway s_{α} , velocity v_{α} ,

5 and relative velocity with the preceding vehicle $\Delta v_{\alpha} = v_l - v_{\alpha}$ as:

$$f_{\text{human}}(v_{\alpha}, \Delta v_{\alpha}, s_{\alpha}) = a[1 - (\frac{v_{\alpha}}{v_0})^{\delta} - (\frac{s^{\star}(v_{\alpha}, \Delta v_{\alpha})}{s_{\alpha}})^2] + \varepsilon$$
(1)

6 where ε is an exogenous noise term designed to mimic stochasticity in human driving behaviors

7 and s^* is the desired headway of the vehicle denoted by:

$$s^{\star}(\nu_{\alpha}, \Delta \nu_{\alpha}) = s_0 + \max(0, \nu_{\alpha}T + \frac{\nu_{\alpha}\Delta\nu_{\alpha}}{2\sqrt{ab}})$$
⁽²⁾

8 and s_0 , v_0 , T, δ , a, b are fixed parameters set in accordance with (23) and provided in Table 1. This 9 model is assigned to all vehicles following the leading trajectory when simulating *human-driven*

10 (baseline) responses to varying downstream conditions, while in *mixed-autonomy* simulations, ev-

ery $\frac{100}{p}$ th vehicle is assigned an AV model to mimic a penetration rate of p%. 11 Figures 3 (top) and 4 (top) depict the platoon response of human-driven vehicles following 12 a sample of the aforementioned trajectories exhibiting some degree of sharp oscillations in driving 13 behaviors. Seen here, perturbations induced by the leading vehicle are amplified by following 14 vehicles within the platoon and propagate backwards in space and forwards in time, resulting in 15 the formation of stop-and-go like behaviors that inhibit the energy-efficiency of the given network. 16 We present in the following section a method for mitigating said oscillations via knowledge of the 17 state of downstream traffic. 18

19 METHODOLOGY

In this section, we present a feedback control strategy that exploits downstream traffic-state estimation data to harmonize driving speeds amongst vehicles while maintaining safe and appropriate gaps between AVs and their leaders. This controller adopts and extends prior heuristic on traffic flow harmonization (17-19, 21), which posit that traffic may be homogenized near its desirable *uniform* driving speed by operating a subset of vehicles near accurate predictions of said speed. We demonstrate the effectiveness of this approach at reducing energy emissions in the following section.

27 Controller design

28 We begin by designing a velocity-based control strategy that, similar to CACC systems, attempts

29 to adjust its response when future driving speeds are expected to reduce sharply. This prediction,

30 however, must satisfy the following conditions:

 It must be achieved without shared communication between adjacent vehicles, as in mixed-autonomy settings human-driven vehicles are incapable of sharing their desired

1	speeds. Instead, we rely on traffic state data, and in particular estimates of average
2	driving speeds $v_{avg}(t) \in \mathbb{R}^m$ spanning across <i>m</i> segments located in positions $x_{avg} \in \mathbb{R}^m$.
3	2. It must regulate its spacing in a manner that is both safe and responsive to the formation
4	of large gaps. In particular, when provided traffic state information overestimate or
5	underestimate the actual state of traffic, additional feedback mechanisms must produce
6	a response more similar to adaptive cruise control (29). We discuss the safety component
7	further in the following subsection.

8 According to the above requirements, the designed velocity includes three parts: the desired 9 velocity; the headway error; and the speed difference, as Eq. (3) depicts:

$$v_d = v_{des} + k_p * (h - h_{des}) + k_d * (v_l - v)$$
(3)

where v_{des} is the desired speed estimated by Eq. (4); *h* is the time gap between the preceding vehicle and the subject vehicle; h_{des} is the desired time headway; v_l and *v* are the speed of preceding vehicle and the subject vehicle respectively and k_p and k_d are gain values.

The desired speed is estimated contingent on the headway between the subject vehicle and preceding vehicle. When the headway is relatively small, we focus on microscopic range, while when the headway is large, we focus on the macroscopic range. The relation between the two is smoothly weighted as follows.

$$v_{\rm des} = \begin{cases} v & \text{if } 0 \le h < 1 \\ (2-h)v + (h-1)v_{\rm avg} & \text{if } 1 \le h \le 2 \\ v_{\rm avg} & \text{if } h > 2 \end{cases}$$
(4)

where v_{avg} is the average speed of the forward traffic estimated by Eq. (5) and the rest of the variables follow the definitions from the above equations.

The average speed of the downstream traffic can be obtained in a convolution way. Specifically, we choose the uniform kernel to estimate it:

$$v_{\rm avg} = \frac{\int_{x_0}^{x_0+w} v_{x_i}}{w}$$
(5)

22

where x_0 is the position of the subject vehicle; *w* is the width of the estimation window and v_{x_i} is the corresponding vehicle at the position x_i .

The second and third term of the Eq. (3) is similar with the design of the ACC vehicle model (*30*). This design intends to capture the human-like car following behavior so that the subject vehicle can maintain a reasonable gap from the preceding vehicle. Equipped with the first term, our controller tries to drive smoothly while maintains reasonable gap with the anticipation of future oscillations in driving speeds.

30 Safety filter

31 To avoid any potential collisions with the preceding vehicle, we add a safety filter to the proposed

32 controller. Our safety filter design is inspired by the simple idea that the gap between the preceding

33 vehicle and the subject vehicle should be larger than the minimum space gap and the headway

34 between the two vehicles should also be larger than the minimum time headway. We start with the

- 1 time headway requirement and add a heuristic in terms of the space gap requirement. The upper
- 2 bound of the velocity determined by safety filter design is calculated by Eq. (6)

$$v_{\rm fs} = \frac{s - s_{\rm min} + v_l \tau_s + \frac{1}{2} a_l \tau_s^2 - \frac{1}{2} v \tau_s}{h_{\rm min} + \frac{1}{2} \tau_s} \tag{6}$$

3 where *s* is the space gap between the preceding vehicle and the subject vehicle; s_{\min} is the mini-4 mum space gap between the two vehicles; τ_s is the decision making horizon; a_l is the acceleration 5 of the preceding vehicle²; h_{\min} is the minimum time headway between the two vehicles and the 6 rest of the variables follow the definitions from the above equations.

7 The detailed design procedure is as follows: Eq. (7) shows the requirement on time head-8 way at time $t = t + \tau_s$.

$$\frac{x_l(t+\tau_s) - x(t+\tau_s)}{v(t+\tau_s)} \ge h_{\min}$$
(7)

where $x_l(t + \tau_s)$ is the position of the preceding vehicle at time $t + \tau_s$; $x(t + \tau_s)$ is the position of the subject vehicle at time $t + \tau_s$; $v(t + \tau_s)$ is the speed of the subject vehicle at time $t + \tau_s$ and the rest of the variables follow the definitions from the above equations. Following simplified dynamics of motion, the position of each the ego and preceding vehicles at time $t + \tau_s$ is:

$$x_l(t+\tau_s) = x_l(t) + v_l(t)\tau_s + \frac{1}{2}a_l(t)\tau_s^2$$
(8)

$$x(t + \tau_s) = x(t) + v(t)\tau_s + \frac{1}{2}a(t)\tau_s^2$$
(9)

9 where a(t) is the target decision variable, and for a fixed desired speed across the decision-making 10 horizon may be expressed as:

$$a(t) = \frac{v_{\rm des} - v(t)}{\tau_s} \tag{10}$$

11

14

12 Plugging in Eq. (8), Eq. (9), and Eq. (10) to solve Eq. (7), we can get an initial upper bound 13 of *v*:

$$v \le \frac{s + v_l \tau_s + \frac{1}{2} a_l \tau_s^2 - \frac{1}{2} v \tau_s}{h_{\min} + \frac{1}{2} \tau_s}$$
(11)

We also want to take the space gap requirement into consideration and get a slightly tighter upper bound. To achieve this, we add an heuristic by replacing the *s* in Eq. (11) with $s - s_{min}$ which leads to our final design of the safety filter velocity as Eq. (6) shows.

18 Combine the velocity design and safety filter, our final controller can be expressed as:

$$v_{c} = \max(0, \min(\underbrace{v_{des}}_{V_{des}} + \underbrace{k_{p} * (h - h_{des}) + k_{d} * (v_{l} - v)}_{Controller \ design}, \underbrace{v_{fs}}_{Safety \ filter}))$$
(12)

19

20 NUMERICAL RESULTS

21 In this section, we present numerical results for the proposed controller across several simulations

22 of the previously described environment. These results aim to answer the following:

 $^{^{2}}$ While multiple estimates for this acceleration may be assigned in practice, we TODO.

Parameter	Description	Value
k_p	Proportional gain	2.0
k_d	Differential gain	0.5
$h_{ m des}$	Desired time headway	2.0 s
W	Sliding window length for speed estimation	3000 m
<i>s</i> _{min}	Minimum safe space headway	5.0 m
h_{\min}	Minimum safe time headway	0.5 s
$ au_s$	Safety decision-making horizon	5.0 s

TABLE 2: Proposed controller parameters.

- Is the proposed controller effective at improving the energy-efficiency and homogeneity 1 of driving across both human-driven and automated vehicles? 2
- 3 • Is this approach sensitive to unforeseen events that are common within multi-lane highway networks, and in particular to disturbances induced by sudden and/or aggressive lane 4 5 changing behaviors?

Simulation procedure 6

Simulations were conducted on the one-lane environment described above with a step size of 0.1 7 sec/step and a following platoon consisting of 200 vehicles. Among the drives recorded within 8 Interstate I-24, we evaluate our method on trajectories that were collected during morning peak 9 demand intervals (6am - 7am) and exhibit some degree of sharp oscillations in driving speeds. This 10 amounts to a total of 10 varying trajectories, seven of which, we note, observe what may deemed as 11 light-to-moderate congestion (e.g. Figure 3), whereby vehicles alternate between free-flowing and 12 congested states of traffic, while the remaining three exhibit more severe forms of congestion (e.g. 13 Figure 4), whereby driving speeds are consistently slow and stop-and-go behaviors are frequent. 14 15 To model an AV penetration rate of 4% we replace every 25th vehicle model in the platoon with the controller depicted in the previous section. The parameters of this controller used within this 16 assessment are depicted in Table 2. 17 To capture realistic traffic state estimation measurements within the above simulations, we 18 19 synchronize the above trajectories real world estimates collected from Inrix. Historical average

- speed measurements are collected from Inrix for the target network, and these values are adjusted 20 in position and time with the leading vehicle to produce results similar to those expected in real 21 world settings. These measurements are collected in segments of length approximately equal to 22
- 0.5 miles, and are updated in increments of 5 minutes. 23

24 **Performance metrics**

25 We evaluate the response of vehicles within the above simulation across the following metrics:

- 1. Energy Efficiency. Improving energy efficiency can incentivize more uniform, and on 26 average slower driving speeds. To analyze the performance of the proposed controller in 27 terms of energy efficiency, we adopt a semi-principled energy model that has a physics-28 based component (22). The model takes as inputs the instantaneous vehicle speed v, 29 30
 - acceleration a, and road grade θ , and outputs engine speed, engine torque, fuel con-

			Distance traveled (km)	MPG (AVs)	MPG (total)
Light/Moderate	Experiment 1	Human-driven Mixed-autonomy	13.71 13.60 (-0.80%)	- 49.87 (+9.82%)	45.41 52.76 (+16.19%)
	Experiment 2	Human-driven Mixed-autonomy	13.863 13.77 (-0.65%)	- 42.55 (+7.86%)	39.45 43.48 (+10.22%)
	Experiment 3	Human-driven Mixed-autonomy	14.58 14.47 (-0.75%)	- 44.93 (+11.32%)	40.36 46.66 (+15.61%)
	Experiment 4	Human-driven Mixed-autonomy	14.09 14.04 (-0.35%)	- 48.21 (+19.15%)	40.46 51.17 (+26.47%)
	Experiment 5	Human-driven Mixed-autonomy	13.23 13.16 (-0.53%)	- 46.14 (+4.41%)	44.19 45.11 (+2.08%)
	Experiment 6	Human-driven Mixed-autonomy	14.24 14.2 (-0.28%)	- 46.24 (+16.21%)	39.79 48.16 (+21.04%)
	Experiment 7	Human-driven Mixed-autonomy	14.48 14.36 (-0.83%)	48.12 (+24.50%)	38.65 49.31 (+27.58%)
Heavy	Experiment 8	Human-driven Mixed-autonomy	13.32 13.31 (-0.08%)	- 42.95 (+17.13%)	36.67 41.42 (+13.50%)
	Experiment 9	Human-driven Mixed-autonomy	13.10 13.00 (-0.76%)	- 52.48 (+44.41%)	36.34 48.69 (+33.98%)
	Experiment 10	Human-driven Control	10.70 10.61 (-0.84%)	38.48 (+24.25%)	30.97 36.03 (+16.34%)
	Average	Human-driven Mixed-autonomy	13.53 13.45 (-0.58%)	- 46.0 (+17.3%)	39.20 46.3 (+18.0%)

TABLE 3: Performance of both fully human-driven and mixed-autonomy simulations, individually and average across 10 runs for each leading experiment/trajectory. Our controller consistently produces driving behaviors that significantly improve the energy-efficiency to both human-driven and automated vehicles at virtually no cost to vehicle miles traveled.



FIGURE 2: Accepted space headway and time by human-driven and automated vehicles in each of the fully human-driven and mixed-autonomy simulations, respectively. As we can see, automated vehicles primarily maintain reasonable headways that distributionally match those of human-driven vehicles but are willing to adopt larger gaps when required to avoid future anticipated congestion.

- 6 2. Throughput. Since the simulation experiment will end if it reaches the end of the
 7 leading trajectory, regulation on controlled vehicles may reduce the throughput near and
 8 upstream of these vehicles. For fixed regions, measuring the distanced traveled can be
 9 an equivalent representation of measuring the traffic flow. Therefore, we use controlled
 10 vehicles' travel distance as a representation of the throughput.
- Proximity to leader. Close proximity may denote unsafe driving behaviors while large distances between vehicles may denote reductions in throughput and may encourage cut-ins and cut-outs by following vehicles. We use time headway and space gap as the metrics to measure the proximity to leader.

15 Comparative analysis

Table 3 depicts the average performance of the system on all 10 utilized trajectories for the met-16 rics we described above. We can see significant improvement on energy efficiency at little cost 17 to the throughput of the system. Comparing to the baseline, the proposed controller provides on 18 average 18.0% savings to energy consumption with only 0.58% reduction on distance travelled 19 by the controlled vehicle. As Figure 2 shows, the controlled vehicles leave a more conservative 20 gap with the preceding vehicle. In controlled cases, both space headway and time headway spread 21 22 in a wider range. With the knowledge of the congestion at downstream, the controlled vehicles should deliberately leave more gap to avoid sharp deceleration, as a result, drive in a smoother 23 24 speed and save energy consumption. This behavior propagates to other vehicles immediately up-25 stream of the automated vehicles as well, resulting in more uniform driving speeds throughout the platoon. This is for instance true in Figure 3, where AVs dampen the magnitude of oscillations 26 experienced by consecutive vehicles within the platoon. In contrast, oscillations in driving speeds 27 in fully human-driven setting are amplified by trailing drivers within the platoon, resulting in the 28

29 subsequent formation of stop-and-go traffic.

30 Sensitivity to lane changes

Finally, we evaluate the ability of our approach to cope with external and unforeseen disturbances 31 common to multi-lane networks. In particular, knowing that our method mitigates congestion 32 33 in part by forming large gaps with leading vehicles when predicted forward speeds are low, we explore the sensitivity of our solution to lane changing events when AVs form large gaps with their 34 immediate leaders. In order to do so, we use a simple lane change model inspired by the work 35 of (31) that stochastically inserts vehicles into the network when the headway between adjacent 36 vehicles is high and periodically removes vehicles to maintain approximate consistency with the 37 38 total number of vehicles within a simulation.

Figure 5 depicts the spatio-temporal performance of human-driven and automated vehicles when lane changes of the form above are introduced into the simulation environments. As we can see, while more frequent oscillations are observed in the presence of lane changes, AVs continue to produce uniform driving amongst vehicles in the mixed-autonomy settings, providing an on average 9.84% MPG improvement among all 10 experiments. The stochastic injection of vehicles does



FIGURE 3: A sample response from sporadic perturbations induced by a leading trajectory. **Top**) Perturbations are amplified by trailing drivers within the platoon and result in frequent transitions between free-flowing and congested states of traffic. **Bottom**) This response is effectively mitigated in the mixed-autonomy setting, with AVs harmonizing driving speeds amongst vehicles.



FIGURE 4: A sample response from frequent perturbations induced by a leading trajectory. **Top**) The strength of severity of oscillations from the leading vehicle produce frequent stop-and-go responses from those upstream. **Bottom**) By maintaining speeds near the aggregate state of the network, AVs are capable of negative many of these stop-and-go responses.



FIGURE 5: A sample response from sporadic perturbations induced by a leading trajectory and the simple lane change model.

- 1 not result in vehicle-to-vehicle collisions either, demonstrating the effectiveness of the proposed
- 2 safety filter as well. We leave analyses of this control strategy under more elaborate lane change
- 3 models for future work.

4 CONCLUSION

- 5 This paper explores the problem of designing congestion mitigation control strategies through au-
- 6 tomated vehicles. We depict a simple feedback control strategy that utilizes downstream traffic
- 7 state information to plan and coordinate a smoother driving trajectory for the purpose of harmo-
- 8 nizing driving speeds and improving energy efficiency. Evaluated with simulations that capture
- 9 high degree of variability in driving behaviors and traffic state estimates common to real-world
- 10 networks, our proposed method could achieve an average of over 15% energy savings with only
- 11 4% AVs introduced to the simulated Interstate I-24 network. Future works can include extending
- 12 this with more accurate and robust simulations of traffic flow dynamics, and devising methods for
- 13 performing similar congestion mitigation without the need for downstream traffic state estimates.

14 ACKNOWLEDGEMENTS

- 15 This material is based upon work supported by the U.S. Department of Energy's Office of En-
- 16 ergy Efficiency and Renewable Energy (EERE) award number CID DE-EE0008872. The views
- 17 expressed herein do not necessarily represent the views of the U.S. Department of Energy or the
- 18 United States Government.

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