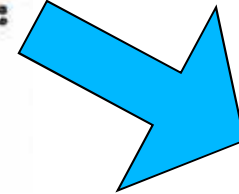
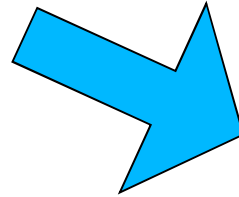


Modeling of Human Response to Ground Motion using Discrete and Continuous Methods



Brenda Dix and Jack Reilly
CE 291F: Control and Optimization of Distributed Parameters Systems
Final Project
May 4, 2010

Motivation For Project

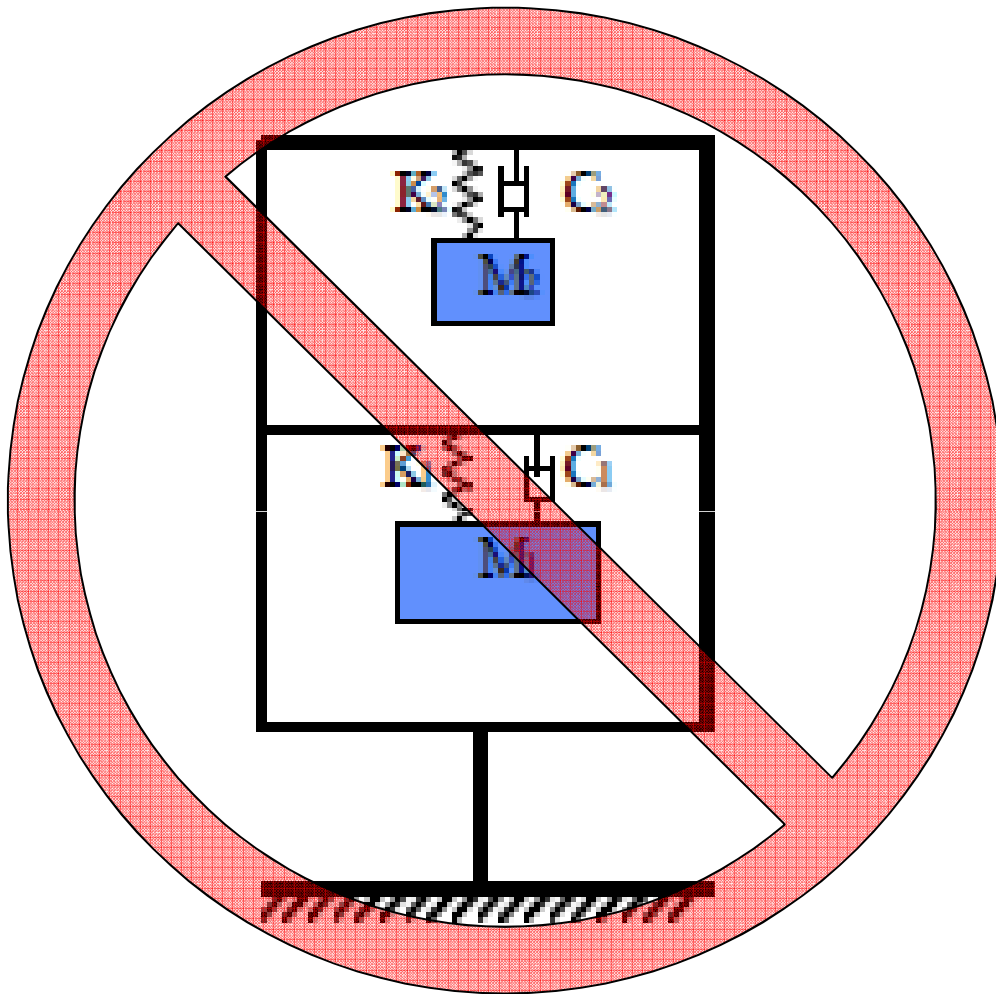


- Using cell phones as sensors for earthquakes
- Effects of human response to rigidly-attached accelerometer signal
- Extraction of ground acceleration from sensor



Discrete Models

ISO standards dictate a vibration simulator of 2DOF systems connected by a rigid frame

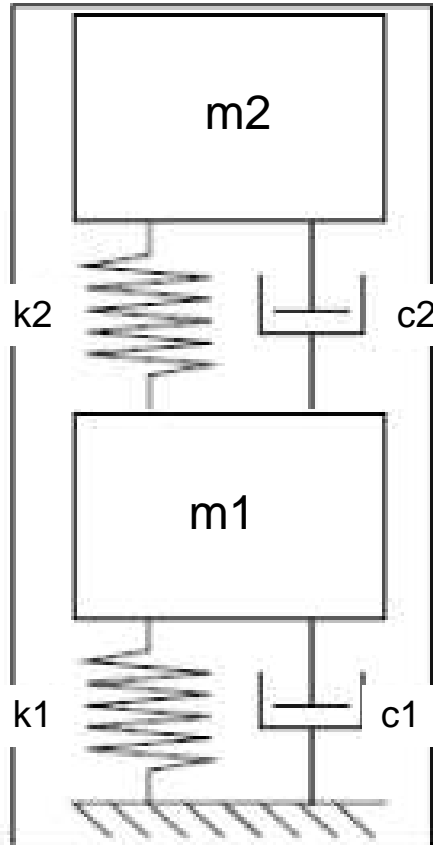


Problems with System:

- Not really 2 DOF – just 2 SDOF systems connected by rigid frame
- Suggests that head and torso move independently of the lower body
- Doesn't account for building motion different from ground motion

Better Discrete Models

Damped 2DOF Model

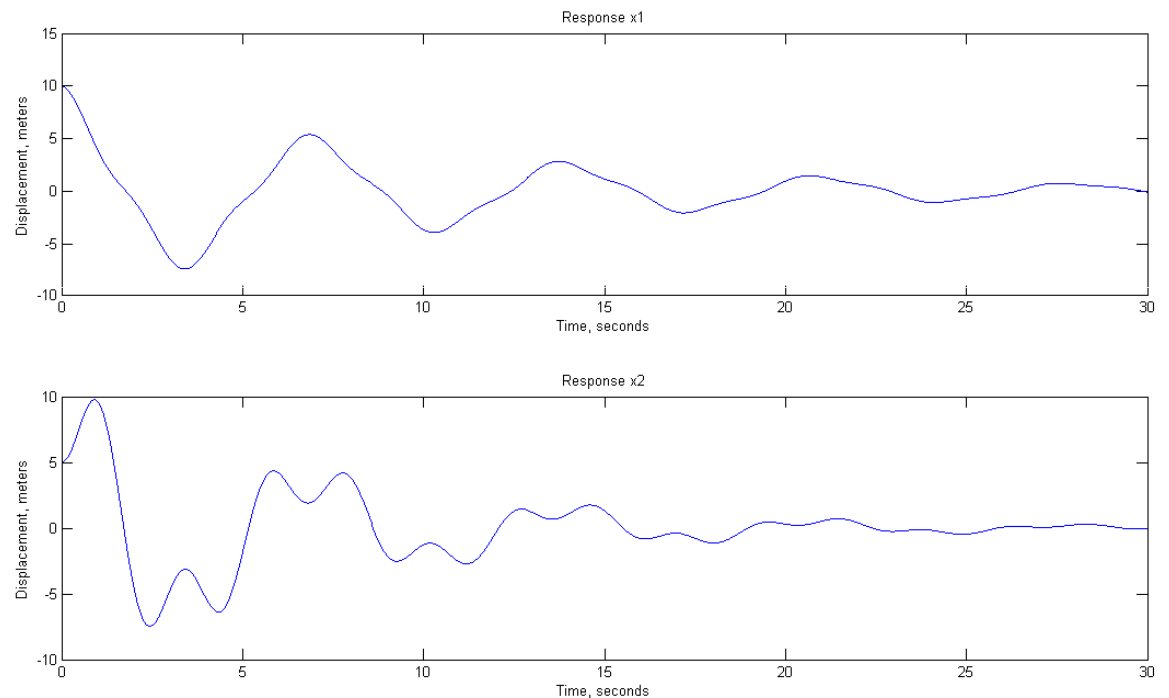


Problems:

- Hard to estimate parameters
- Doesn't account for building motion separate from ground motion
- Still a discrete model

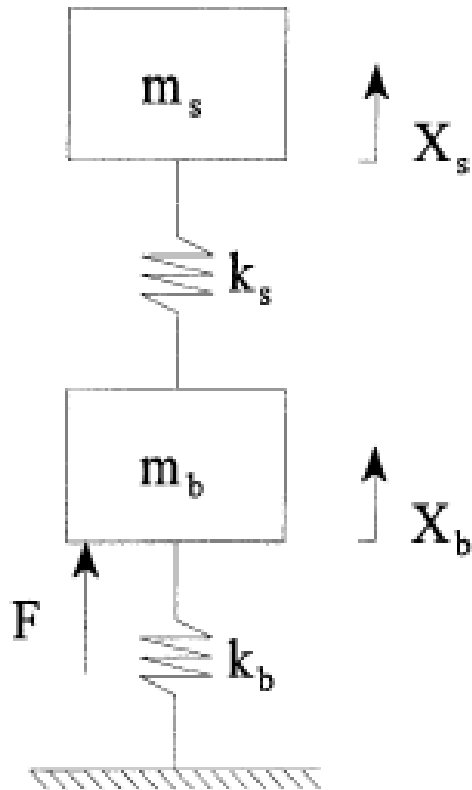
$$m_1 \ddot{x}_1 + (c_1 + c_2) \dot{x}_1 - c_2 \dot{x}_2 + (k_2 + k_1)x_1 - k_2 x_2 = 0$$

$$m_2 \ddot{x}_2 + c_2 (\dot{x}_2 - \dot{x}_1) + k_2 (x_2 - x_1) = 0$$



Better Discrete Models Continued

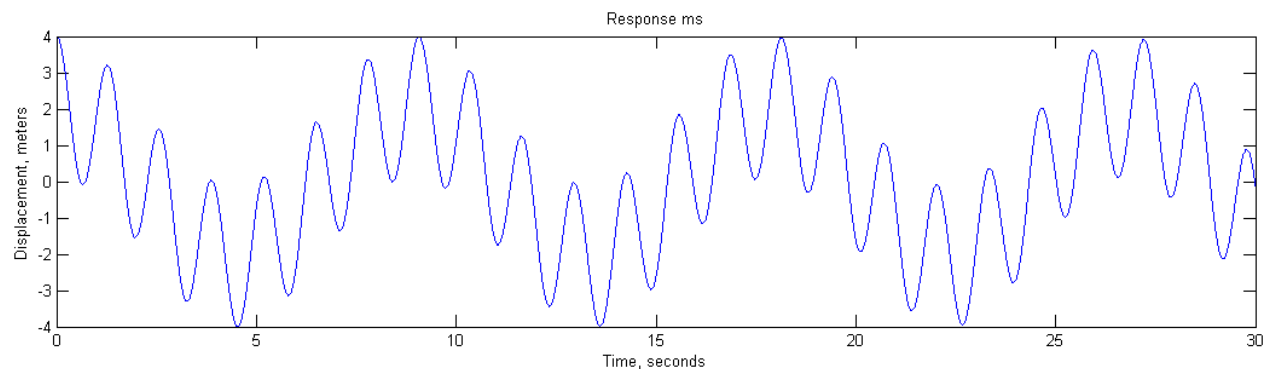
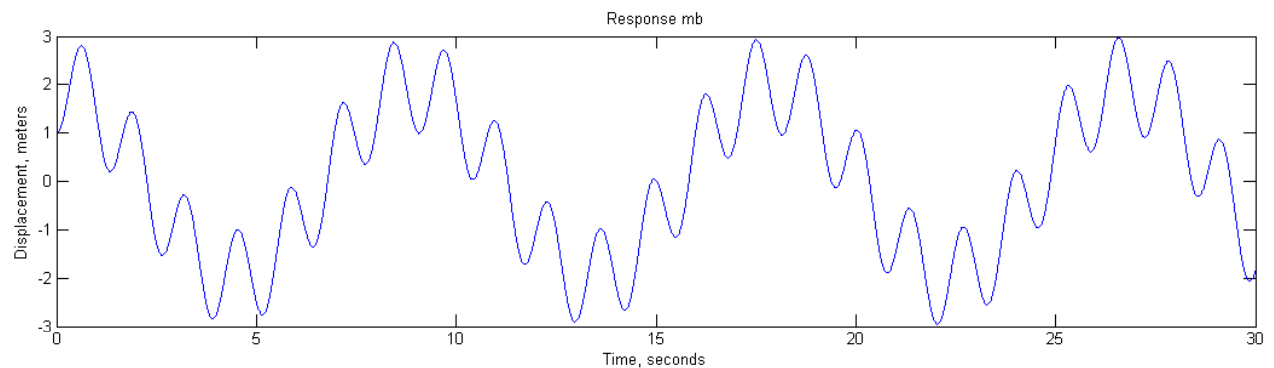
Subject-Beam Model



$$m_s \ddot{X}_s + k_s X_s - k_s X_b = 0$$

$$-k_s X_s + m_b \ddot{X}_b + (k_s + k_b) X_b = F$$

$$\omega_s^2 = \frac{\omega_b^2(\omega_b^2 - \omega^2)}{\omega_b^2 - (1 + \alpha)\omega^2}$$



Problems:

- SDOF – not very robust
- Does not account for damping

Continuous Model

$$m \frac{\partial^2 U}{\partial t^2} - k \frac{\partial^2 U}{\partial x^2} = 0$$

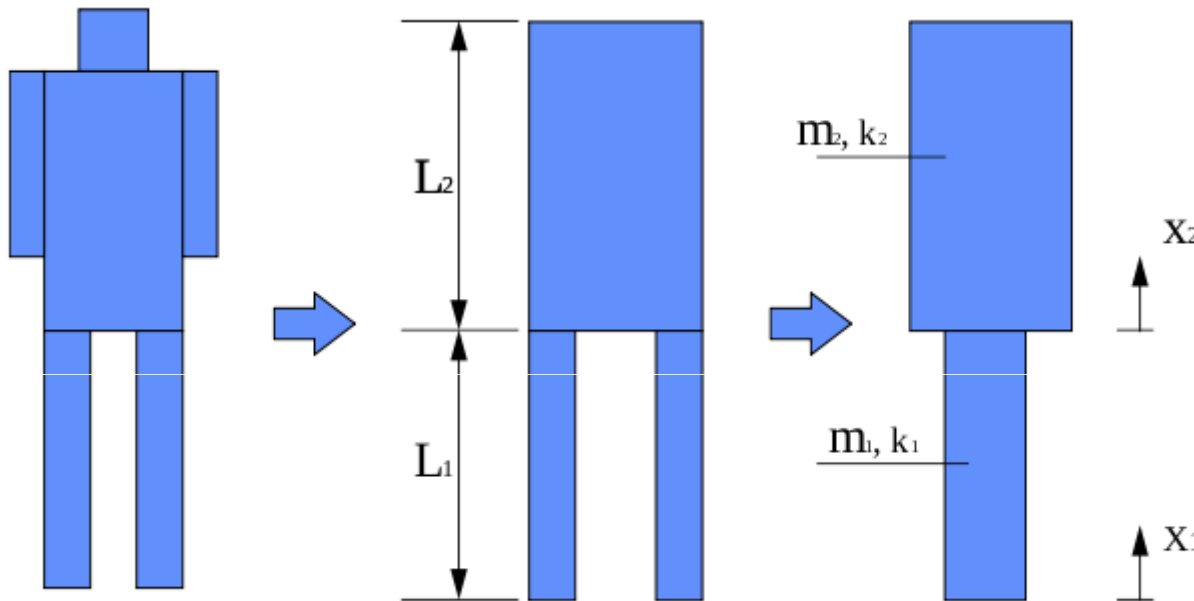
• Two rods with independent properties (mass, length, stiffness)

• Assume $L_1 = L_2$, $m_2 = 2m_1$, and determine stiffnesses

• Force boundary conditions on the system of rods

• Axial Displacement, Forces =

- @ 0, no force
- @ x_1 , no displacement
- @ $x_1 + x_2$,



Solution to PDE System

Separation of Variables

$$u(x, t) = T(t)\Phi(x)$$

Modal Shape

$$\Phi_i(x) = C_i \cos b_i x_i + D_i \sin b_i x_i \quad i = 1, 2$$

Application of BC's

$$\Phi_1(x_1) = D \sin b_1 x_1 \quad 0 \leq x_1 \leq L_1$$

$$\Phi_2(x_2) = D \left\{ \sin b_1 L_1 \cos b_2 x_2 + \sqrt{\frac{m_1 k_1}{m_2 k_2}} \cos b_1 L_1 \sin b_2 x_2 \right\} \quad 0 \leq x_2 \leq L_2$$

Full Model of PDE

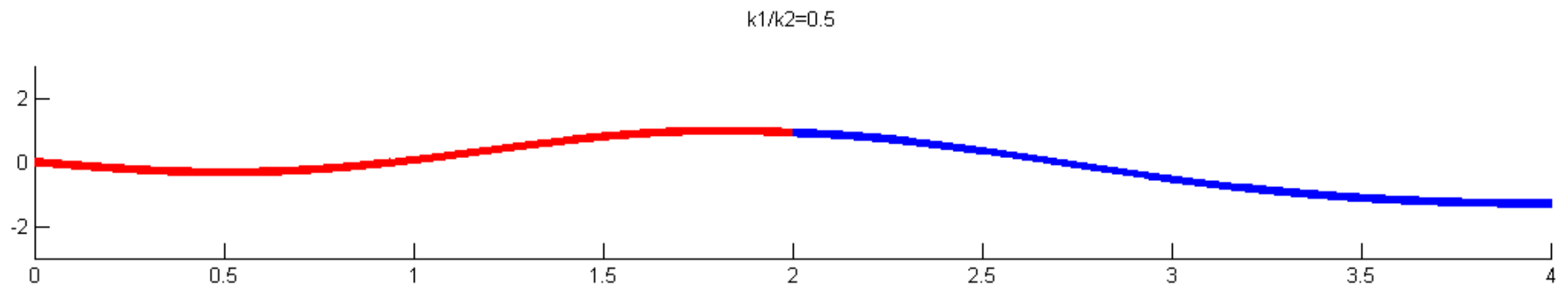
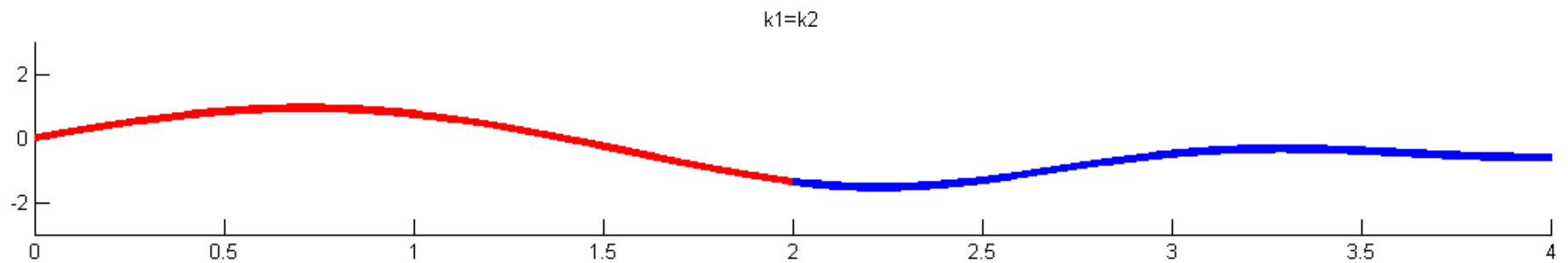
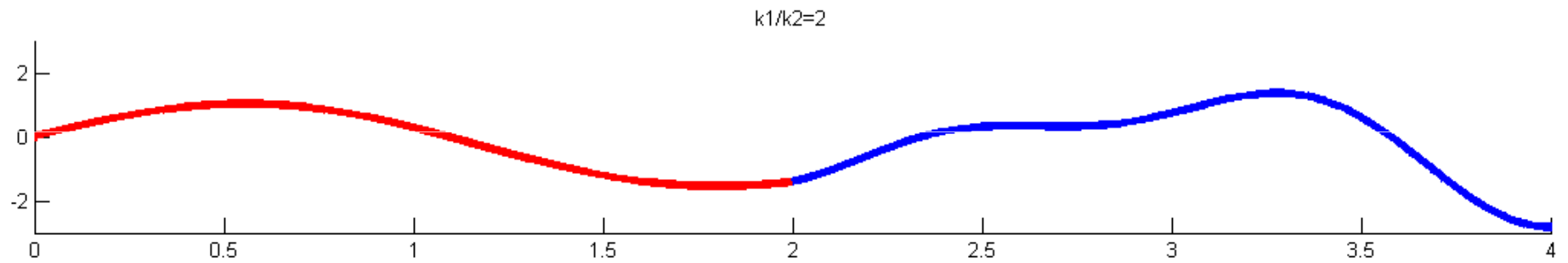
- Stiffness Ratio Selection: for simplicity, a ratio of $k_1 / k_2 = 2$ is chosen
- Initial Conditions
 - No velocity
 - Assume sinusoidal initial shape

$$u(x_1, t) = \sum_{i=0}^n A_i \sin(b_i x_1) \cos(\omega_i t)$$

$$u(x_2, t) = \sum_{i=0}^n A_i \sin(b_i L_1 (1 + \frac{2x_2}{L_2})) \cos(\omega_i t)$$



3 Different Stiffness Ratios



Benefits of Continuous Model

- Reduces the number of parameters to be determined
 - In-between values embedded within the PDE, while discrete requires more nodes (more parameters)
- Can determine relative amplitudes of different modes as a function of location on body.
 - Know most likely position of sensor on human

$$u(x_1, t) = \sum_{i=0}^n A_i \sin(b_i x_1) \cos(\omega_i t)$$

$$u(x_2, t) = \sum_{i=0}^n A_i \sin(b_i L_1 (1 + \frac{2x_2}{L_2})) \cos(\omega_i t)$$

Further Study and Conclusions

FURTHER STUDY

- Additional sensors on the human participant to study local vibrational effects.
- Consider lateral movement and horizontal vibrations in order to understand 3-D picture of earthquake motions.
- Refine experiments to determine system parameters.
- Add damping to the model.

CONCLUSIONS

- Discrete models are commonly accepted but do not provide the resolution needed for the project.
- Our continuous model allows for the calculation of the modal response along the length of the body.
- Our continuous model does not meet our original goal of extraction of the earthquake ground motion signal.

References

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Thanks for listening!

Any questions?

