

# Estimation of State Noise for the Ensemble Kalman filter algorithm for 2D shallow water equations.

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## Introduction

Motivation

## Ensemble Kalman filter algorithm

Constitutive Equations

EnKF algorithm

Some results

## Estimation of state noise

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Navier Stokes equations and assumptions

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Generation of state noise occurrences

## Ensemble Kalman filter on real data

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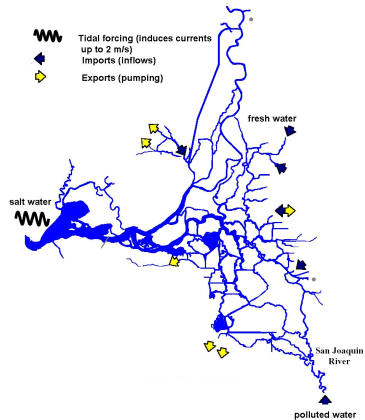
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# Sacramento Delta



# Sacramento Delta

Before the levee breach



# Sacramento Delta

After the levee breach



# Lagrangian sensors

Lagrangian sensors measure their positions as they drift along with the flow.

When trying to solve the two-dimensional shallow water equations, one needs accurate initial and boundary conditions which are usually not available.

Data assimilation of the Lagrangian measurements from the drifters allow to estimate the velocity field in the river even without accurate boundary conditions.

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# Two-dimensional shallow water equations

$$\frac{\partial u}{\partial t} + \vec{U} \cdot \nabla u = -g \frac{\partial \eta}{\partial x} + F_x + \frac{1}{h} \nabla \cdot (h \nu_t \nabla u) \quad (1)$$

$$\frac{\partial v}{\partial t} + \vec{U} \cdot \nabla v = -g \frac{\partial \eta}{\partial y} + F_y + \frac{1}{h} \nabla \cdot (h \nu_t \nabla v) \quad (2)$$

$$\frac{\partial h}{\partial t} + \vec{U} \cdot \nabla h + h \nabla \cdot \vec{u} = 0 \quad (3)$$

where

$$F_x = -\frac{1}{\cos \alpha} \frac{g n^2}{h^{4/3}} u \sqrt{u^2 + v^2}$$

$$F_y = -\frac{1}{\cos \alpha} \frac{g n^2}{h^{4/3}} v \sqrt{u^2 + v^2}$$

$h$ : total water depth

$\vec{U} = (u, v)$ : velocity field

$\eta$ : free surface elevation

$\nu_t$ : turbulent diffusion coefficient

$\alpha = \alpha(x, y)$ : bottom slope

$n$ : Manning coefficient.

## Two-dimensional shallow water equations

Boundary conditions:

$$u(x, y, t)|_{\partial\Omega_{\text{land}}} = 0, \quad v(x, y, t)|_{\partial\Omega_{\text{land}}} = 0, \quad (4)$$

$$(u(x, y, t), v(x, y, t))|_{\partial\Omega_{\text{upstream}}} = f(x, y, t), \quad (5)$$

$$\eta(x, y, t)|_{\partial\Omega_{\text{downstream}}} = g(x, y, t), \quad (6)$$

Initial conditions:

$$u(x, y, 0) = u_0, \quad v(x, y, 0) = v_0, \quad h(x, y, 0) = h_0, \quad (7)$$

# Drifter model

$$\frac{dx_{D_i}(t)}{dt} = u(x_{D_i}(t), y_{D_i}(t), t), \quad (8)$$

$$\frac{dy_{D_i}(t)}{dt} = v(x_{D_i}(t), y_{D_i}(t), t), \quad (9)$$

# State Augmentation

We use state augmentation to simplify the observation model

$$\theta_n = \begin{pmatrix} u(t_n) \\ v(t_n) \\ h(t_n) \\ x_D(t_n) \\ y_D(t_n) \end{pmatrix} \quad (10)$$

# Forward model

$$\theta_{n+1} = F_n(\theta_n) + w_n. \quad (11)$$

$F_n$ : one time step in the discretized shallow water and drifter model.

$\theta_{n+1}$ : predicted system state at time  $t_{n+1}$ .

$w_n$ : state noise (modeling error between the reality and the 2D model).

$Q_n$ : covariance of the state noise.

# Observation model

$$y_n = C_n \theta_n + \epsilon_n. \quad (12)$$

$y_n$ : measurements from the drifters.

$C_n = (\mathbf{0} \ \mathbb{I})$ : observation model.

$\epsilon_n$ : measurement noise.

$R_n$ : covariance of the measurement noise.

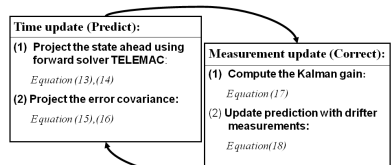
# EnKF Algorithm

1. Initialization: An ensemble of  $N_{\text{states}}$  states  $\xi_0^{(p)}$  indexed by  $p$  are generated to represent the uncertainty in  $\theta_0$ .
2. Time update:

$$\xi_{n|n-1}^{(p)} = F_n(\xi_{n-1|n-1}^{(p)}) + w_{n-1}^{(p)} \quad (13)$$

$$\theta_{n|n-1} = \frac{1}{N_{\text{states}}} \sum_{p=1}^{N_{\text{states}}} \xi_{n|n-1}^{(p)} \quad (14)$$

$$E_{n|n-1} = [\xi_{n|n-1}^{(1)} - \theta_{n|n-1}, \dots, \xi_{n|n-1}^{(N_{\text{states}})} - \theta_{n|n-1}] \quad (15)$$



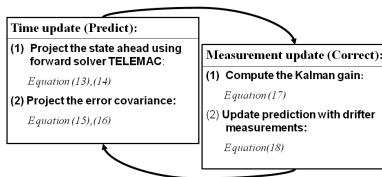
# EnKF Algorithm

## 3. Measurement update:

$$\Gamma_{n|n-1} = \frac{1}{N_{\text{states}} - 1} E_{n|n-1} E_{n|n-1}^T \quad (16)$$

$$K_n = \Gamma_{n|n-1} C_n^T (C_n \Gamma_{n|n-1} C_n^T + R_n)^{-1} \quad (17)$$

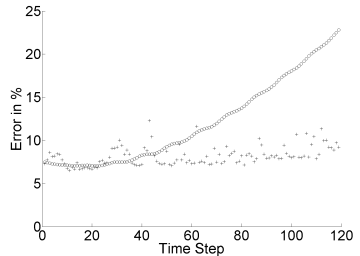
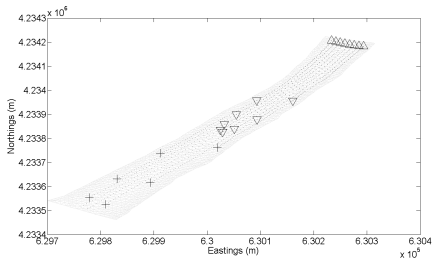
$$\xi_{n|n}^{(p)} = \xi_{n|n-1}^{(i)} + K_n (y_n - C_n \xi_{n|n-1}^{(p)} + \epsilon_n^{(p)}) \quad (18)$$





## Twin experiment results

Drifters are released using a software and the EnKF algorithm runs using those measurements.



# Limitations

The state noise used here is realistic for twin experiments, since we know the discrepancy between the "reality" and the model, as they are both from the same software.

We need more realistic state noise in order to have the algorithm run with the real data from November experiment.

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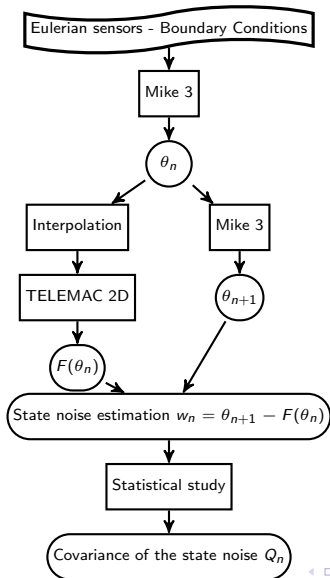
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# Navier-Stokes equations

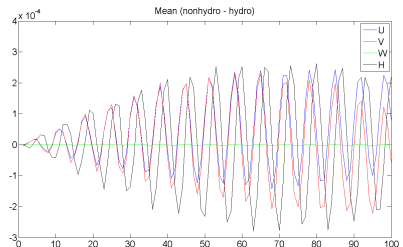
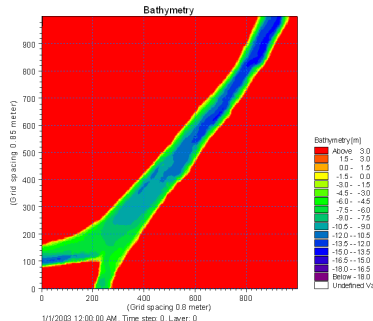
$$\frac{1}{\rho c_s^2} \frac{\partial P}{\partial t} + \frac{\partial u_j}{\partial x_j} = SS \quad (19)$$

$$\begin{aligned} \frac{\partial u_i}{\partial t} + \frac{\partial(u_i u_j)}{\partial x_j} + 2\Omega_{ij} u_j &= -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + g_i \\ + \frac{\partial}{\partial x_j} (\nu_T \{ \frac{\partial u_i}{\partial x_i} + \frac{\partial u_j}{\partial x_j} \} - \frac{2}{3} \delta_{ij} k) &+ u_i SS \end{aligned} \quad (20)$$

# Testing the hydrostatic assumption

Hydrostatic assumption: pressure in the river can be estimated using the hydrostatic pressure.

Valid for  $\frac{L}{H} \gg 1$ , where  $L$  is the horizontal characteristic length of the river.

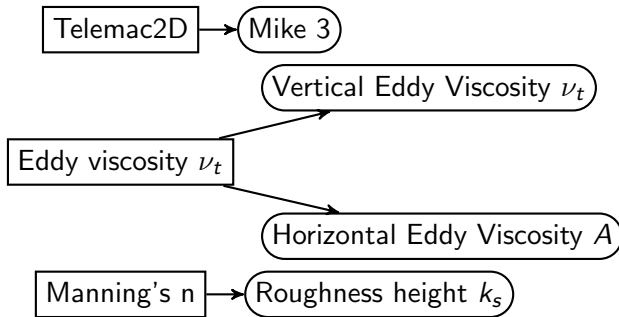


# Navier-Stokes equations using hydrostatic assumption

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \quad (21)$$

$$\begin{aligned} \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial vu}{\partial y} + \frac{\partial wu}{\partial z} = & -g \frac{\partial \eta}{\partial x} - \frac{1}{\rho_0} \frac{\partial p_a}{\partial x} - \frac{g}{\rho_0} \int_z^\eta \frac{\partial \rho}{\partial x} dz \\ & - \frac{1}{\rho_0 h} \left( \frac{\partial s_{xx}}{\partial x} + \frac{\partial s_{xy}}{\partial y} \right) + F_u + \frac{\partial}{\partial z} \left( \nu_t \frac{\partial u}{\partial z} \right) \end{aligned} \quad (22)$$

$$\begin{aligned} \frac{\partial v}{\partial t} + \frac{\partial uv}{\partial x} + \frac{\partial v^2}{\partial y} + \frac{\partial wv}{\partial z} = & -g \frac{\partial \eta}{\partial y} - \frac{1}{\rho_0} \frac{\partial p_a}{\partial y} - \frac{g}{\rho_0} \int_z^\eta \frac{\partial \rho}{\partial y} dz \\ & - \frac{1}{\rho_0 h} \left( \frac{\partial s_{yx}}{\partial x} + \frac{\partial s_{xy}}{\partial y} \right) + F_v + \frac{\partial}{\partial z} \left( \nu_t \frac{\partial v}{\partial z} \right) \end{aligned} \quad (23)$$



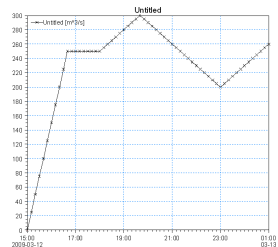
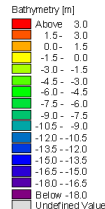
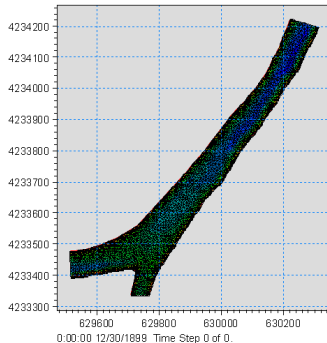
**Figure:** Equivalence of parameters between the two dimensional and the three dimensional models.

A relationship between the roughness height and the Manning's  $n$  can be found as:

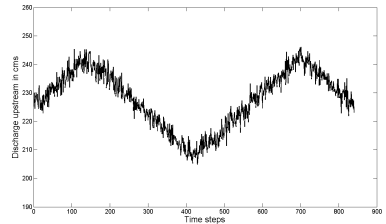
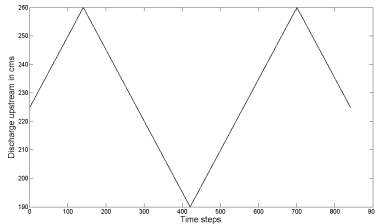
$$n = \frac{k_s^{\frac{1}{6}}}{25.4} \quad (24)$$

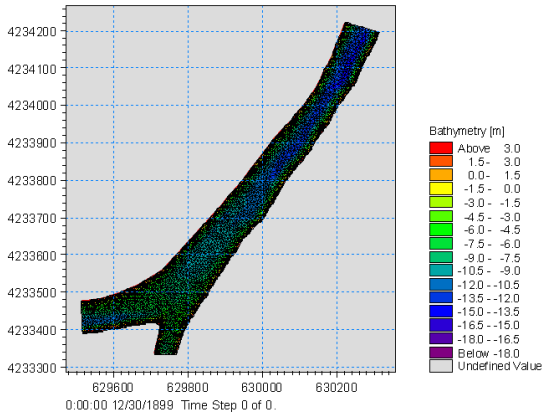


# Three dimensional simulations

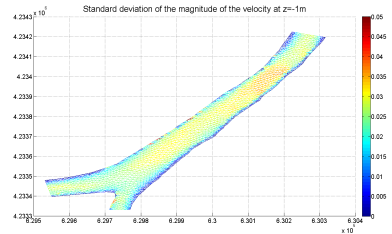
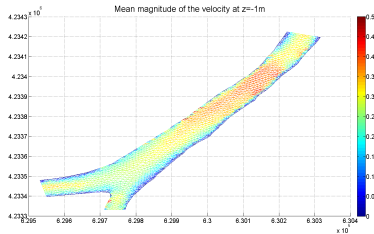


# Boundary conditions

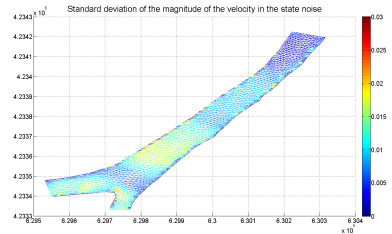
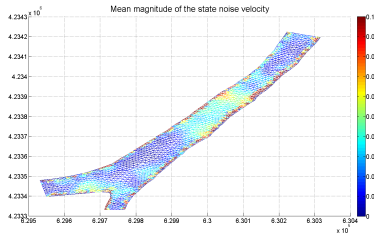




# Result of the 3D simulation



# State noise characteristics



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# Real data



# Cross validation principle

No data are available to validate.

- ▶ Remove 1 or 2 drifters from the data set.
- ▶ Run the EnKF on the remaining drifters.
- ▶ Compute the trajectory of the extracted drifters using the estimated velocity field.
- ▶ Compare it with the real trajectory.



# Future work

- ▶ Run the EnKF using the real data set and the generated state noise.
- ▶ Generate a state noise model for the drifters.

# Questions?

