

THE TRANSPORT EQUATION:

ANALYTICAL SOLUTION AND APPLICATION FOR A
CONTROL PROBLEM

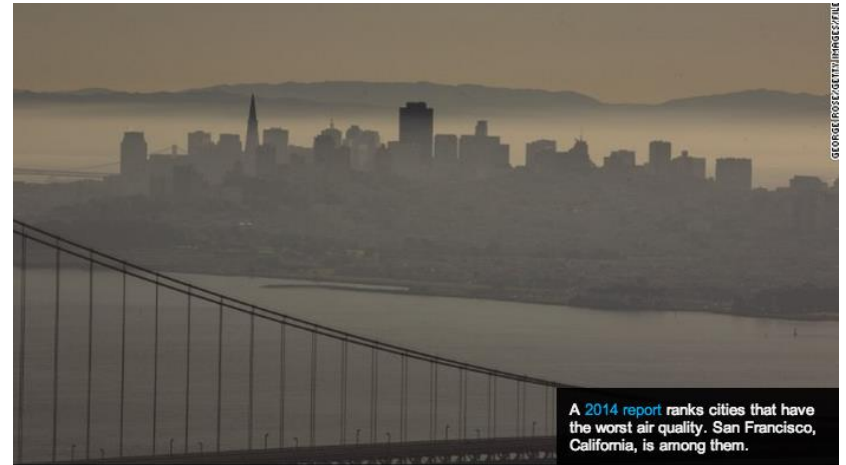
CE291 Term Project

Di Jin

Zeshi Zheng

Motivation and Strategy

- Predict air pollutant concentration by solving 2D transport equation
- Apply the solution to a control problem



Advection-Dispersion Equation

$$\frac{\partial c}{\partial t} = D_L \frac{\partial^2 c}{\partial x^2} + D_T \frac{\partial^2 c}{\partial y^2} - \frac{u \partial c}{\partial x} - \frac{v \partial c}{\partial y} + q(x, y, t)$$

Initial condition: $c(x, y, 0) = f(x, y)$.

C: solute concentration.

D_L, **D_T**: the longitudinal and transverse dispersion coefficients

u, **v**: wind speed in the x and y direction

q: a source/sink term

Overview of Solving Strategy

- Non-dimensionalization
- Transformation

$$\frac{\partial c}{\partial T} = \frac{\partial^2 c}{\partial X^2} + \frac{\partial^2 c}{\partial Y^2} + Q(X, Y, T)$$

- Analogy of Green's Function
- Fourier Transform of Green's Function
- Solution of Green's Function

- *Ref: Aral, Mustafa M., and Boshu Liao. "Analytical solutions for two-dimensional transport equation with time-dependent dispersion coefficients." Journal of Hydrologic Engineering 1.1 (1996): 20-32.*

Non-Dimensionalization

$$x = \frac{x}{L}, \quad y = \frac{y}{L}, \quad D_L = \frac{D_L}{D_r}, \quad D_T = \frac{D_T}{D_r},$$

$$t = \frac{t D_T}{D_r}, \quad u = \frac{u L}{D_r}, \quad v = \frac{v L}{D_r}, \quad c = \frac{c}{c_r}, \quad q = \frac{q L^2}{c_r D_r}, \quad f(x, y) = \frac{f(x, y)}{c_r}$$

$$\frac{\partial c}{\partial t} = \frac{D_L \partial^2 c}{\partial x^2} + \frac{D_T \partial^2 c}{\partial y^2} - \frac{u \partial c}{\partial x} - \frac{v \partial c}{\partial y} + q(x, y, t)$$

Assumptions and Transformation

Assume $D_L = a^2 D_T = D$, and D scales with L^2/T , we have:

$$\frac{L_x^2}{T} = \frac{a^2 L_y^2}{T} \quad \text{and} \quad L_x = a L_y$$

$$x' = x, \quad y' = ay, \quad v' = av$$

Let $X = x' - ut$, $Y = y' - v't$

$$\frac{\partial c(x', y', t)}{\partial t} = \frac{\partial c(X, Y, t)}{\partial t} + (-u) \frac{\partial c}{\partial X} + (-v') \frac{\partial c}{\partial Y}$$

Introduce T :

$$T = \alpha(t) = \int_0^t D dt' = D * t$$

$$\frac{\partial c}{\partial t} = \frac{\partial c}{\partial T} \frac{\partial T}{\partial t} = D \frac{\partial c}{\partial T}$$

Assumption and Transformation

$$\frac{\partial c}{\partial T} = \frac{\partial^2 c}{\partial X^2} + \frac{\partial^2 c}{\partial Y^2} + Q(X, Y, T)$$

Where:

$$Q(X, Y, T) = \frac{q\{X + U\alpha^{-1}(T), \frac{[Y + V\alpha^{-1}(T)]}{a}, \alpha^{-1}(T)\}}{D[\alpha^{-1}(T)]}$$

Initial condition:

$$c(X, Y, 0) = f\left(X, \frac{Y}{a}\right), -\infty < X, Y < \infty$$

Green's Function

- Our Equation

$$\frac{\partial c}{\partial T} = \frac{\partial^2 c}{\partial X^2} + \frac{\partial^2 c}{\partial Y^2} + Q(X, Y, T)$$

- Heat equation with sources on an infinite domain

$$\frac{\partial u}{\partial t} = k\nabla^2 u + Q(\mathbf{x}, t)$$

- Green's Function for the heat equation without boundaries satisfies

$$\frac{\partial G}{\partial t} = k\nabla^2 G + \delta(\mathbf{x} - \mathbf{x}_0)\delta(t - t_0)$$

subject to:

$$G(\mathbf{x}, t; \mathbf{x}_0, t_0) = 0 \quad \text{for } t < t_0$$

- To solve this, apply Fourier Transform. The reason is it will transform the PDE into an ODE, which is much easier to solve.

Fourier Transform

- Introduce Fourier Transform of the Green's Function

$$\bar{G}(\boldsymbol{\omega}, t; \mathbf{x}_0, t_0) = \frac{1}{(2\pi)^n} \int_{-\infty}^{\infty} G(\mathbf{x}, t; \mathbf{x}_0, t_0) e^{i\boldsymbol{\omega} \cdot \mathbf{x}} d^n x$$

$$G(\mathbf{x}, t; \mathbf{x}_0, t_0) = \int_{-\infty}^{\infty} \bar{G}(\boldsymbol{\omega}, t; \mathbf{x}_0, t_0) e^{-i\boldsymbol{\omega} \cdot \mathbf{x}} d^n \boldsymbol{\omega}$$

- Transforming $\frac{\partial G}{\partial t} = k \nabla^2 G + \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0)$ gives

$$\frac{\partial \bar{G}}{\partial t} = -k\omega^2 \bar{G} + \frac{e^{i\boldsymbol{\omega} \cdot \mathbf{x}_0}}{(2\pi)^n} \delta(t - t_0)$$

- For $t > t_0$

$$\frac{\partial \bar{G}}{\partial t} = -k\omega^2 \bar{G}$$

- Solving this we will have:

$$\bar{G} = C(\boldsymbol{\omega}) e^{-k\omega^2(t-t_0)}$$

Fourier Transform

- From $G(\mathbf{x}, t; \mathbf{x}_0, t_0) = 0$, for $t < t_0$
- Integrate $\frac{\partial \bar{G}}{\partial t} = -k\omega^2 \bar{G} + \frac{e^{i\omega \cdot \mathbf{x}_0}}{(2\pi)^n} \delta(t - t_0)$ from $t = t_{0-}$ to $t = t_{0+}$

$$\bar{G}(\boldsymbol{\omega}, t; \mathbf{x}_0, t_0) = 0 \quad \text{for } t < t_0$$

$$\bar{G}(t_{0+}) = \frac{e^{i\boldsymbol{\omega} \cdot \mathbf{x}_0}}{(2\pi)^n}$$

$$\bar{G}(\boldsymbol{\omega}, t; \mathbf{x}_0, t_0) = \frac{e^{i\boldsymbol{\omega} \cdot \mathbf{x}_0}}{(2\pi)^n} e^{-k\omega^2(t-t_0)}$$

$$G(\mathbf{x}, t; \mathbf{x}_0, t_0) = \frac{1}{(2\pi)^n} \left[\frac{\pi}{k(t-t_0)} \right]^{\frac{n}{2}} e^{\frac{-(\mathbf{x}-\mathbf{x}_0)^2}{4k(t-t_0)}}$$

- From conversion between u and G :

$$u(\mathbf{x}, t) = \int_0^t \int_{-\infty}^{\infty} \left[\frac{1}{4\pi k(t-t_0)} \right]^{\frac{n}{2}} e^{\frac{-(\mathbf{x}-\mathbf{x}_0)^2}{4k(t-t_0)}} Q(\mathbf{x}_0, t_0) d^n \mathbf{x}_0 dt_0 + \int_{-\infty}^{\infty} \left(\frac{1}{4\pi k t} \right)^{\frac{n}{2}} e^{\frac{-(\mathbf{x}-\mathbf{x}_0)^2}{4k t}} f(\mathbf{x}_0) d^n \mathbf{x}_0$$

where n is the number of dimensions

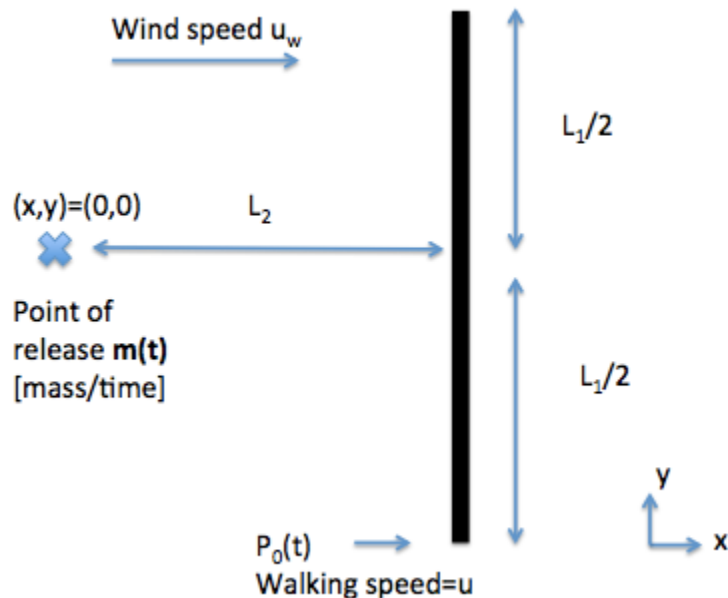
Solution

- Point Source Transport:

$$C(x, y, t) = \frac{M}{4\pi Dt} \exp \left[-\frac{(x - Ut)^2 + (y - Vt)^2}{4Dt} \right]$$

where M is the mass of the release.

Control Problem-Definition



- Factory releasing pollutants at $m(t)$
- Number of people entering the road during the day $P_0(t)$
- Health impact
 - cost function

$$\int_{t_0}^{t_f} \int_{-L_1/2}^{L_1/2} c(y, t) * p(y, t) dy dt$$

- Want: $m(t)$ that minimizes the cost function
 - Constraints:

$$\int_{t_0}^{t_f} m dt = M, \quad m \leq m_{max}$$

Analytical Approach

1) Superposition to model continuous source

$$c(x, y, t)_{instant_point} = \frac{M}{4\pi Dt} \exp\left(-\frac{(x - u_x t)^2}{4Dt}\right) \exp\left(-\frac{(y - u_y t)^2}{4Dt}\right)$$

$$c(x, y, t)_{continuous} = \int_{t_0}^t \frac{m(t')}{4\pi Dt'} \exp\left(-\frac{(x - u_x t')^2}{4Dt'}\right) \exp\left(-\frac{(y - u_y t')^2}{4Dt'}\right) dt'$$

Substituting $x = L_2$, $u_x = u_w$, $u_y = 0$:

$$c(y, t)_{continuous} = \int_{t_0}^t \frac{m(t')}{4\pi Dt'} \exp\left(-\frac{(L_2 - u_w t')^2}{4Dt'}\right) \exp\left(-\frac{y^2}{4Dt'}\right) dt'$$

Analytical Approach

2) Rewrite the cost function (product of number of people and concentration, integrated over time and space):

$$\int_{t_0}^{t_f} \int_{-L_1/2}^{L_1/2} c(y, t) * p(y, t) dy dt$$

Applying method of characteristics, we obtain:

$$p(y, t) = p\left(t - \frac{(y + \frac{L_1}{2})}{u}\right)$$

We can rewrite the cost function as:

$$\int_{t_0}^{t_f} \int_{-\frac{L_1}{2}}^{\frac{L_1}{2}} \left(\int_{t_0}^t \frac{m(t')}{4\pi Dt'} \exp\left(-\frac{(L_2 - u_w t')^2}{4Dt'}\right) \exp\left(-\frac{y^2}{4Dt'}\right) dt' \right) * p\left(t - \frac{(y + \frac{L_1}{2})}{u}\right) dy dt'$$

Numerical Approach- Discretization

Superposition principle: treat continuous release as i individual releases of m_i at infinitesimal time intervals δt , where $\delta t = 24 \text{ hr} / i$

$$\text{total exposure} = \sum_{i=1}^{i=k} m_i \delta t * k_i$$

$$\text{where } k_i = \sum_{t_i=i\delta t+\delta t}^{t_i=t_f} \sum_{y_j=-L_1/2}^{y_j=L_1/2} \frac{1}{4\pi D(t_i - i\delta t)} \exp\left(-\frac{(L_2 - u_w(t_i - i\delta t))^2}{4D(t_i - i\delta t)}\right) \exp\left(-\frac{y_j^2}{4D(t_i - i\delta t)}\right) p\left(t_i - \frac{(y_j + \frac{L_1}{2})}{u}\right) \delta t \delta y$$

(Recall the cost function:)

$$\int_{t_0}^{t_f} \int_{-\frac{L_1}{2}}^{\frac{L_1}{2}} \left(\int_{t_0}^t \frac{m(t')}{4\pi D t'} \exp\left(-\frac{(L_2 - u_w t')^2}{4D t'}\right) \exp\left(-\frac{y^2}{4D t'}\right) dt' \right) * p\left(t - \frac{(y + \frac{L_1}{2})}{u}\right) dy dt'$$

Numerical Approach- Discretization

$$\text{total exposure} = \sum_{i=1}^{i=k} m_i (\delta t * k_i)$$

constant
↓

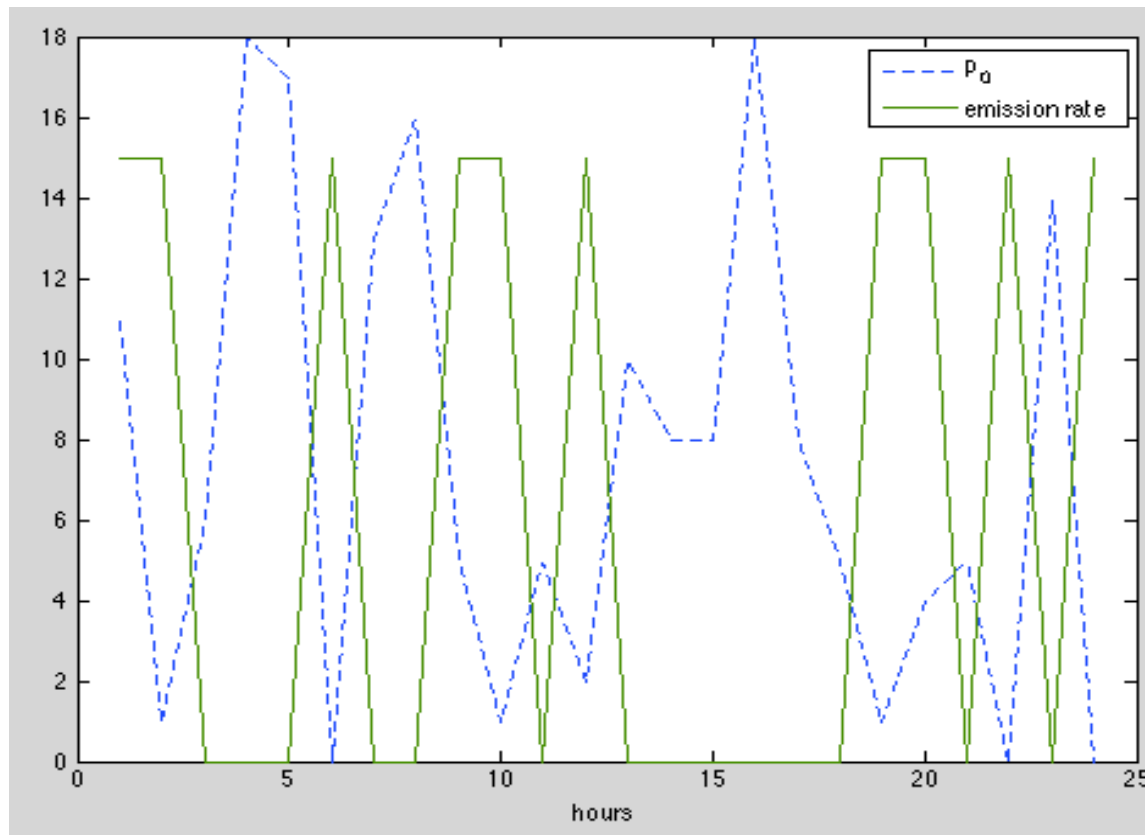
Recall the constraints: $\int_{t_0}^{t_f} m dt = M, m \leq m_{max}$

Solution: rank k_i from smallest to largest, then assign m_{max} to m_i in this order until $\sum_{i=1}^{i=k} m_i \delta t * k_i = M$

Numerical Solution

Given:

$u=100$; $u_w=10$; $D=100$; $L_1=1000$; $L_2=200$; $m_{\max}=15$; $M=150$; $\delta t=1$; $\delta y=u*\delta t=100$;
 P_0 generated by random function



References

- Aral, M. M., & Liao, B. (1996). Analytical Solutions for Two-Dimensional Transport Equation with Time-Dependent Dispersion Coefficient. *Journal of Hydrologic Engineering*, 1:20-32.
- Prentice-Hall, Inc. (1987). *Elementary Applied Partial Differential Equations (2nd ed.)*. New Jersey: Richard Haberman